Cooling, Ageing and Condition Monitoring of Electric Traction Machines

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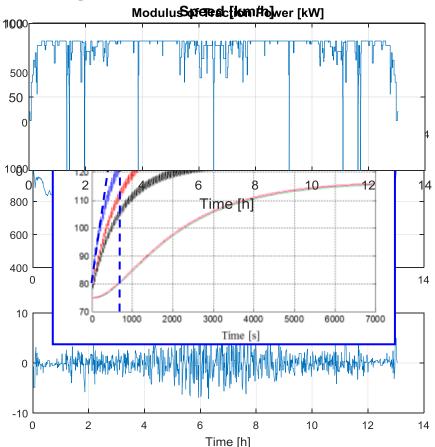
Heavy Duty Trucks

- Daily travel distance > 800 km
- 30..90 tons
- Full Electric now possible
 - On batteries, with "Mega" Charging
 - On Electric Roads
- What about the electric drive trains?



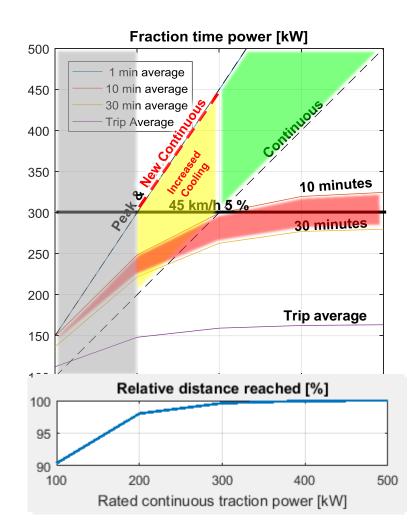
Full Electric Heavy Duty Trucks

- High power levels, during extended periods
 - Significant cooling requirements
- HDT in a tough Long Haul cycle:
 - 44 ton
 - 500/750 kW traction power (cont/peak)
 - 13 h operation roundtrip
 - Max 60 [s] average Power = 651 [kW]
 - Max 600 [s] average Power = 325 [kW]
 - Max 1800 [s] average Power = 280 [kW]
 - Full trip average
 Power = 163 [kW]
- Is that reasonable?



Less power?

- Try 100...500 kW CONTINUOUS – ... with 150...750 kW PEAK
- Assume thermal time constant 10...30 minutes
 - Assume >300 kW for performance
 - < 200 kW underperforms</p>
 - 200...300 kW enough, but overheating may occur ...
 - >> 300 kW overperforms?
- Lower power with Increased Cooling may be interesting
 - 5...10 % less energy consumption



What happens at overload?

- Core losses change moderately
- Stator winding losses increase dramatically!
 - $P_{windingloss} = R \times I^2$
- Heat generation > cooling capability



Increased Cooling ...?

- Air cooling outside
- Water sleeve cooling
- Oil cooling, also on end winding and maybe inside rotor
- Oil cooling directly on the windings
- Cooling inside the stator windings
- Cooling inside the stator conductors

Peak Power determined by direct winding cooling capability

Deak Power determined by

capacitance

thermal



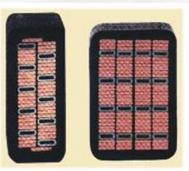
Short end-winding

High fill factor

Cooling gaps

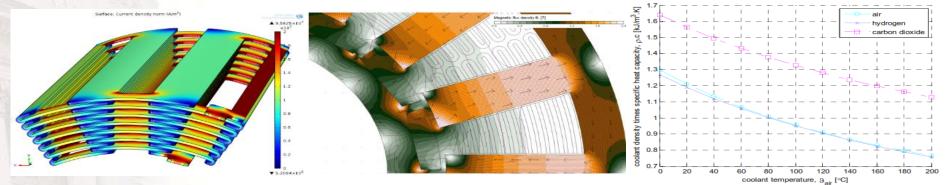






First idéa: - The laminated winding

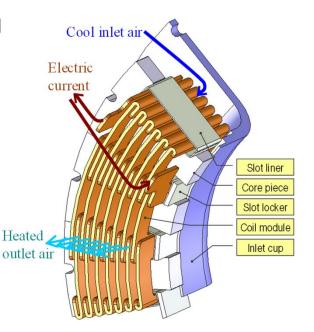
- Suitable cooling media ?
- Air a reasonable compromise

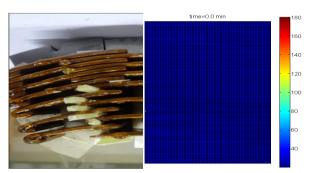


| | Air | | Hydrogen | | Carbon Dioxide | | Water | | Transformer Oil | |
|------------------------------|----------|----------|----------|----------|----------------|--------------|----------|----------|-----------------|-------|
| Temperature [C] | 20 | 120 | 20 | 120 | 20 | 120 | 20 | 120 | 20 | 120 |
| heat capacity [kJ/kg,K] | 1,005 | 1,014 | 14,2 | 14,49 | 0,854 | 0,938 | 4,187 | 4,25 | 1,71 | 2,114 |
| Mass Density [kg/m3] | 1,204 | 0,898 | 0,084 | 0,063 | 1,83 | 1,364 | 999,6 | 942,2 | 879,1 | 816,5 |
| Cooling Potential [kJ/m3,K] | 1,21 | 0,91 | 1,19 | 0,91 | 1,56 | <i>1,2</i> 8 | 4 185 | 4 004 | 1 503 | 1 726 |
| Thermal Conductivity [W/m,K] | 0,026 | 0,033 | 0,178 | 0,227 | 0,016 | 0,024 | 0,594 | 0,686 | 0,111 | 0,102 |
| Dynamic Viscosity [Pa s] | 1,80E-05 | 2,30E-05 | 8,00E-06 | 1,10E-05 | 1,40E-05 | 1,90E-05 | 1,00E-03 | 2,00E-04 | 0,052 | |

Directly cooled laminated windings

- Provide direct cooling & overloading capability
- Excellent cooling capability
- Manufacturing problems lead to Overheated & undercooled regions





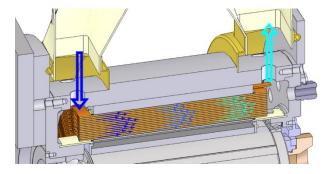
3 \ Axially Stacked IPMSM

- Axially displaced laminated windings
- Moulded core facilitates construction BUT <u>limits torque</u>, increases leakage and AC losses in the winding
- Narrow cooling channels, high flow and cooling demand – small geometric differences results large discrepancy in temperature

| Stator size D _o /D _i -H | mm | 200/120-224 |
|---|-------------------|-------------|
| Speed n, nom/pk | krpm | 7.5/15 |
| Current I _{ph} , nom/pk | А | 120/400 |
| <u>Torque</u> T _{em} , nom/pk | Nm | 35/125 |
| C density J _{ph} ,nm/pk | A/mm ² | 7.0/21.2 |

3\overrightaryon Modular Segmented SPMSM

- Tangentially displaced laminated windings
- <u>Existing</u> machine with redesigned windings - Directly Cooled Laminated Fractional Pitch Windings





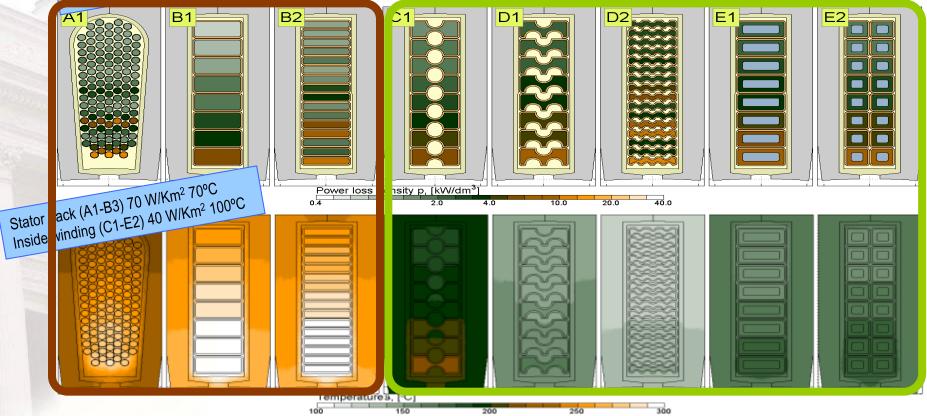


| mm | 240/136-200 |
|-------------------|-----------------|
| krpm | 1.5/6.0 |
| А | 116/300 |
| Nm | 250/500 |
| A/mm ² | 7.0/18.2 |
| | krpm A Nm |

What we learned this far ...

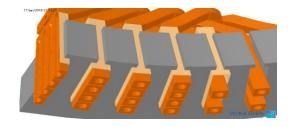
- High current densities (>30 A/mm²) can be balanced by forced air velocity (20-25 m/s) with hot-spot temperature limits (150-180 °C).
- It is VERY hard to manufacture with maintained physical integrity.
- Additional losses due to stray fields near the air gap occur.

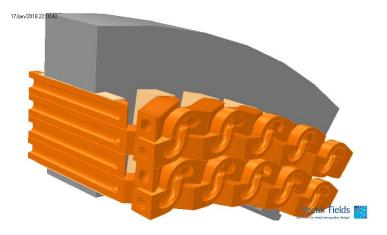
Alternative designs



Directly cooled hollow conductors

- Cooling integration in the machine conductors
- Less challenge with production tolerances and physical integrity
- Mechanical integration: end regions, inlet and outlet



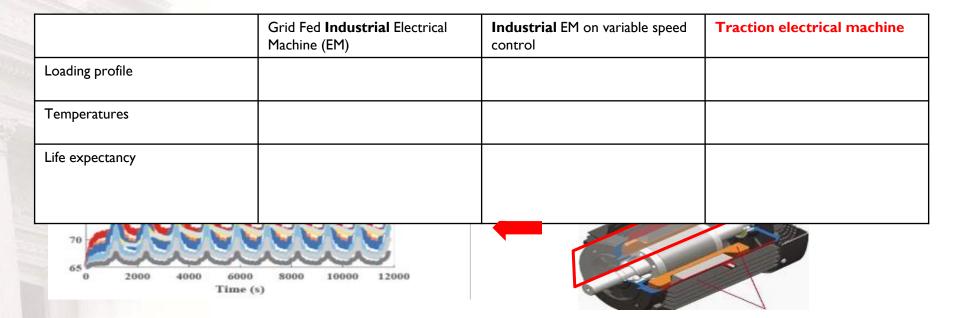


Degradation



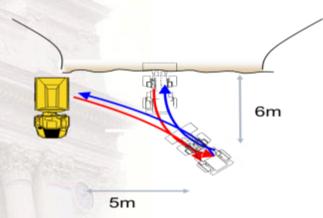
- Degradation of the EIS
 - Degradation and failure of electrical machine
 - Degradation and failure of **electrified vehicle**
- TEAM stresses
 - Thermal
 - Electrical
 - Ambient
 - Mechanical

Dynamic temperatures



(Plot above from Emma Arfa Grunditz, PhD thesis)

Application example – Wheel Loader

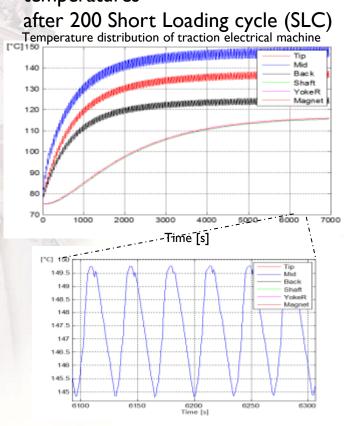


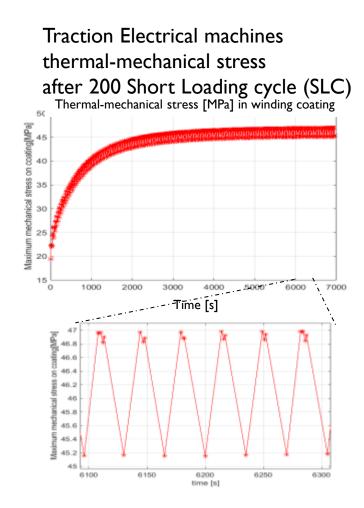


- Four wheel driven by electrical machines
- Short loading cycle (SLC)
 - Filling bucket
 - Leaving pile
 - Towards truck
 - Emptying bucket
 - Leaving truck
 - Toward pile

Traction Electrical machines

temperatures





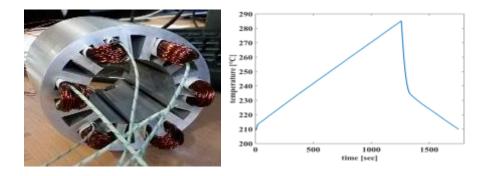
Other examples – thermal cycling

 Voitto Kokko, Fortum, 'Aging Due to Thermal Cycling by Power Regulation Cycles in Lifetime Estimation of Hydroelectric Generator Stator Windings'



| Root cause | Distribution | | |
|---|--------------|--|--|
| Ageing by number of operation hours | 15% | | |
| Ageing by thermal cycling | 38% | | |
| Internal PD & defective corona protection | 27% | | |
| Mechanical condition | 8% | | |
| Vibration | 8% | | |
| Contamination | 4% | | |

 C. Sciascera, University of Nottingham, 'Lifetime Consumption and Degradation Analysis of the Winding Insulation of Electrical Machines'

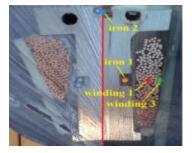


Expected lifetime: 713 hours, Actual lifetime: 90 hours.

Motorrette/stator segment







Full stator

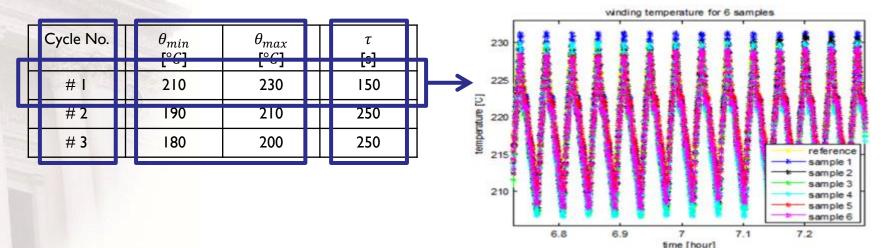
Motorrette/

Stator segment

Impregnation, Thermal sensors

Thermal cycles – tested

- Table shows three tested cycles with 20°C depth
- Plot of measured hot spot temperatures (cycle #1)



Lifetime – simulated VS measured

| | | | • | | | | | |
|---|----------|-----------------------|---|--------|--------|---|--------|---------|
| Γ | Test No. | θ_{cycle} [°C] | Τ | LT 1 | LT 2 | Τ | LT 3 | tested |
| | | | | [hour] | [hour] | | [hour] | [hour] |
| | #1 | 210-230 | | 4255 | 949 | | 30 | <47 |
| Γ | #2 | 190-210 | | 24999 | 4256 | | 119 | 150-180 |
| | #3 | 180-200 | | 64172 | 9456 | | 192 | 250-290 |
| | | | | | | | | |

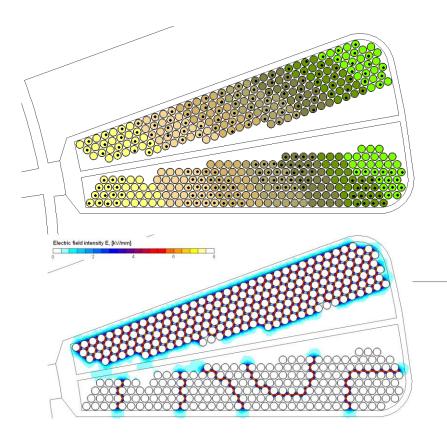
Thermal cycles and corresponding lifetime

- Arrhenius law model over-estimates the lifetime.
- High fatigue model can more accurately predict the lifetime of EIS, when they are exposed to these thermal cycles.
- The high temperature oxidation is not the only degradation mechanism.
- Thermal-mechanical fatigue is one of the degradation mechanisms, which cannot be overlooked.

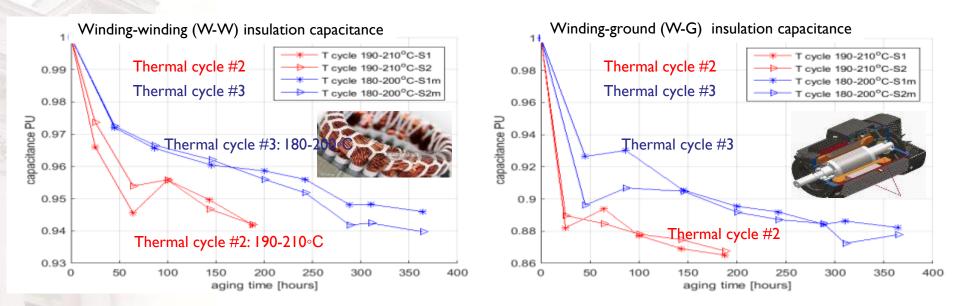
Condition monitoring – concept



- 7 turns with two groups of parallel strands, kept separate or mixed
- Winding-Winding and Winding-Core capacitance measured as a function of thermal cycle ageing



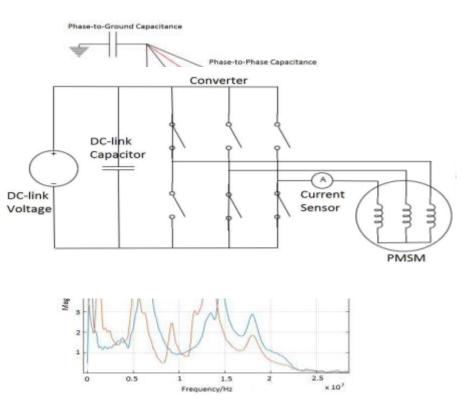
Insulation capacitance



- Thermal cycle #2 <u>190~210°</u> C: 5% to 6% (W-W) and 12 to 14% (W-G) drop
- Thermal cycle #3 <u>180~200°</u> C : 4% to 6% (W-W) and 11 to 12% (W-G) drop

On board condition monitoring

- Use the clear changes of insulation capacitance during aging
- Measure e.g. the winding-core capacitances
 development over time
- Use the power electronic controller on a vehicle;
- By changing between two switching patterns, a voltage pulse over windings is formed;
- High frequency current is measured;
- Migration of amplitude and frequency of the current → parasitic capacitance → the state of health of machine



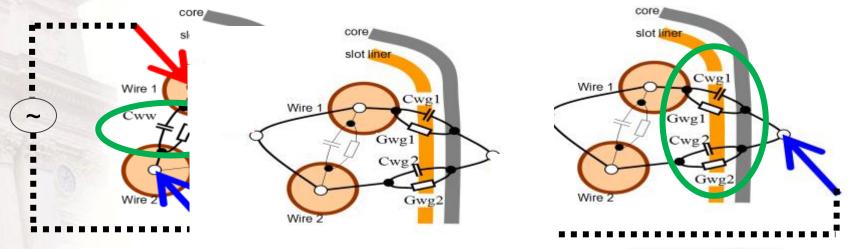
Conclusions

- Traction machines generally sized for a certain overloading
- Efficient direct winding cooling may change overloading conditions and thus sizing
- Thermal cycling drives ageing
- Efficient direct winding cooling may limit thermal cycling and thus extend lifetime
- Parameter measurement for condition monitoring promising technology









Winding-winding



Winding-core

